

# **Development of a compositional PVT model for a multicomponent, multiphase hydrocarbon reservoir**

**Evstafeev Evgeniy Aleksandrovich, Akramov Bakhshillo Shafievich, Shevtsov Vladimir Mikhailovich,  
Turaev Ulugbek Daminovich**

Independent PhD candidate (Doctor of Philosophy in technical sciences), lecturer, Department of oil, gas and gas-condensate field development, Tashkent Branch of Gubkin Russian State University of Oil and Gas (National Research University), Republic of Uzbekistan, Tashkent

Candidate of technical sciences, professor, Department of oil, gas and gas-condensate field development, Tashkent Branch of Gubkin Russian State University of Oil and Gas (National Research University), Republic of Uzbekistan, Tashkent

Doctor of technical sciences (DSc), professor; leading research scientist, Department of field development design and monitoring, JSC "O'ZLITINEFTGAZ", Republic of Uzbekistan, Tashkent

Deputy director for production, Mubarek Oil and Gas Production Department, Republic of Uzbekistan, Mubarek

**ABSTRACT:** This paper presents an algorithm for the construction of a compositional PVT model of reservoir fluids in a multicomponent, multiphase hydrocarbon field. The methodology entails a step-by-step calibration of the differential condensation isotherm and the differential depletion curve for reservoir fluids. The algorithm was validated through the development of a compositional PVT model for the gas cap and oil rim of a gas-condensate field in the Republic of Uzbekistan.

## **I. INTRODUCTION**

Currently, one of the primary challenges in designing the development of multicomponent, multiphase hydrocarbon reservoirs is the accurate prediction of key production metrics that account for in-situ phase behavior under depletion drive. Existing approximate mathematical models based on material balance equations [1], as well as three-phase "black-oil" models [2], fail to capture all complexities encountered in such fields, even when using advanced reservoir simulators. A viable solution for this is compositional hydrodynamic modeling [2].

However, constructing a robust PVT model of the reservoir fluid - one that reproduces laboratory PVT-cell (bomb) data and accurately describes the phase behavior of hydrocarbon mixtures in porous media as remains a formidable objective requiring an integrated approach. Such a model must ensure convergence of critical fluid properties, including saturation pressure, gas deviation (Z) and formation volume factors, standard - condition density, dew - point pressure, and initial condensate yield in reservoir gas [3].

In this research paper we propose an algorithm for the sequential calibration of a compositional PVT model for a gas-condensate mixture and oil-based on the known component composition of the reservoir gas and validated against laboratory measurements.

## **II. METHODOLOGY FOR BUILDING AND TUNING COMPOSITIONAL PVT MODELS OF MULTIPHASE RESERVOIR FLUIDS**

This paper demonstrates two algorithms were developed for building compositional PVT models of reservoir fluids in a multicomponent, multiphase hydrocarbon field.

### Algorithm 1: Compositional Modeling of a Gas-Condensate Mixture

- 1.Import the average reservoir-gas composition - taken from the field development plan - into the simulator's PVT designer.
- 2.Represent the high-boiling  $C_{5+}$  fraction by selecting a homologous alkane from the standard component library whose molecular weight closely matches  $C_{5+}$ .
- 3.Subdivide the  $C_{5+}$  fraction into pseudocomponents using the Whitson correlation [4], spanning from n-hexane ( $C_6H_{14}$ ) to the chosen replacement component. In the first iteration, the correlation's exponent parameter  $\alpha$ —which controls the exponential distribution of pseudocomponent mole fractions—is set to unity by default.
- 4.Perform a constant-volume depletion (CVD) test to simulate depletion drive [1]. Compare the model's dew-point pressure, maximum-condensation pressure, initial and minimum potential condensate yields, condensate density at standard conditions, and gas formation-volume factor against values reported in the field development plan.
- 5.If discrepancies arise, calibrate the PVT model by adjusting one or more of the following parameters:
  - The Whitson exponent  $\alpha$  (allowed range: 0.5–2.5 [5]);
  - The type of correlation used for pseudocomponent critical temperature and acentric factor;
  - The critical temperatures of the first and last pseudocomponents ( $\pm 5\%$  variation);
  - Binary interaction coefficients and volume-shift parameters for pseudocomponents (range:  $-0.25$  to  $+0.25$ ) [6].

### Algorithm 2: Compositional Modeling of Reservoir Oil

- 1.Import the average oil composition from the field development plan, or convert a black-oil model to compositional format using the simulator's built-in tool [2].
- 2.Select homologous alkanes whose molecular weights approximate the key oil fractions.
- 3.Subdivide the heaviest fraction (residuum) into pseudocomponents via the Whitson correlation, ensuring that the total number of components matches the gas-condensate model—this consistency is required by most commercial simulators [6].
- 4.Perform a CVD test on the oil model. Compare the saturation pressure, gas-oil ratio, formation-volume factor, and oil density at standard conditions with reference data from the development plan.
- 5.If the modeled parameters deviate, adapt the model by tuning:
  - The Whitson exponent  $\alpha$  (0.5–2.5);
  - Mole fractions of the first and last pseudo components;
  - Correlation type for pseudo component critical temperature and acentric factor;
  - Volume-shift for high-boiling components;
  - Critical temperature of the high-molecular-weight pseudocomponent;
  - Binary interaction coefficients and volume-shift parameters for pseudocomponents.

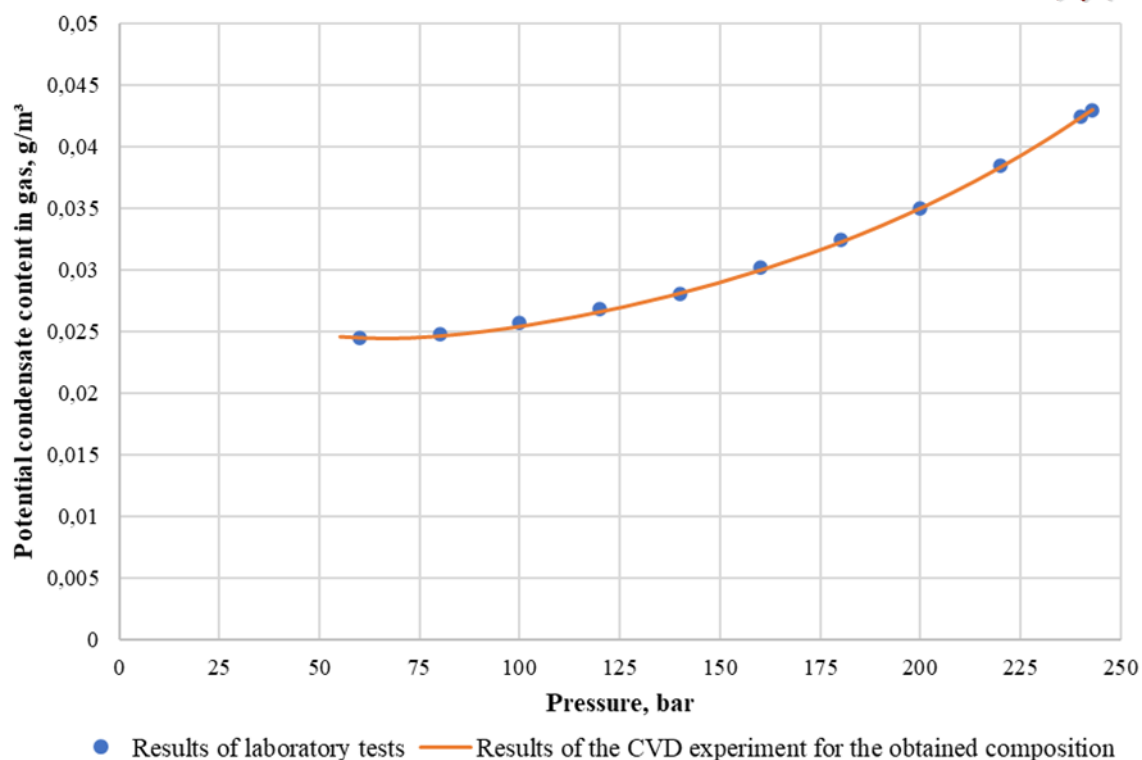
## III. RESULTS

In this research proposed algorithms have been validated using the fluid from one of the gas-condensate fields under development in the Republic of Uzbekistan. The reservoir gas composition for this field is shown in table 1.

Table 1. Composition of the reservoir gas of the studied field

Component	CH <sub>4</sub>	C <sub>2</sub> H <sub>6</sub>	C <sub>3</sub> H <sub>8</sub>	i-C <sub>4</sub> H <sub>10</sub>	n-C <sub>4</sub> H <sub>10</sub>	C <sub>5</sub> H <sub>12+</sub>	N <sub>2</sub>	CO <sub>2</sub>	H <sub>2</sub> S
$X_i$ , %	90,64	3,52	0,81	0,13	0,18	0,91	0,46	3,31	0,04

Note that the molar mass of the  $C_5H_{12+}$  fraction is 113.596 g/mol; therefore, decane ( $C_{10}H_{22}$ ) was selected as the surrogate component for its representation. Following the proposed methodology, decane was then subdivided into pseudocomponents (in this case,  $C_6$  through  $C_{10}$ ). The Whitson correlation exponent  $\alpha$  was tuned to achieve an accurate pseudocomponent distribution, and appropriate correlations were chosen to calculate the critical temperatures, critical pressures, and acentric factors of each pseudocomponent. A constant volume depletion (CVD) experiment was conducted on the resulting fluid mixture. Figure 3.1 presents the differential condensation isotherm at a reservoir temperature of 91°C, comparing the model prediction against laboratory measurements.



**Fig.3.1: Differential condensation isotherm for the reservoir gas of the studied field.**

The reservoir fluid composition shown in Table 1 has been used as the basis for modeling the oil of the studied field. Certain components and their properties have been adjusted based on oil property reports for this reservoir. Specifically, a component labeled F1 has been implemented to represent the residue formed during fractional distillation of the oil. Additionally, some alkane-series hydrocarbons have been modified to better represent the heavy fractions. For example, dodecane ( $C_{12}H_{26}$ ) has been used to simulate the  $C_5+$  heavy component with a molar mass of 163 g/mol, while eicosane ( $C_{20}H_{42}$ ) has been selected to represent component F1 with a molar mass of 256.455 g/mol.

All subsequent steps have been performed in accordance with the previously developed algorithm. As a result, strong convergence has been achieved between the calculated parameters of the reservoir oil and laboratory measurements of oil samples. A comparison of the laboratory and modeled oil parameters for the field under study is presented in table 2.

**Table 2. Comparison of laboratory and modeled oil parameters for the studied field**

№	Parameter	Unit of measurement	Laboratory test results	PVT model calculation after tuning	Deviation, %
1	Saturation pressure	bar	152,9	152,814	-0,056
2	Density at standard conditions	kg/m <sup>3</sup>	892	892,009	0,001
3	Formation volume factor under reservoir conditions	m <sup>3</sup> /m <sup>3</sup>	1,06	1,0589	-0,104
4	Oil gas content (GOR)	m <sup>3</sup> /m <sup>3</sup>	26	25,87	-0,5

As evidenced by table 2 and figure 3.1, application of the proposed algorithms has yielded accurate PVT models for both the oil and gas-condensate fluids of the studied field.

Mobile type cloud kind computing is defacto emerging as the new kind paradigm primarily for aiding the broad kind and range of those multimedia type services [6]. We have presented the layered kind architecture basically for MCC which defacto clears up the respective functions and those of the protocols. We herein suggest forth a connection in handoff kind mechanism basically among the cloud type lets and discuss the related kind resources, which the management premeditated for the challenges for MCC.

#### IV. CONCLUSION

Summing up, this research paper introduces practical algorithms for constructing compositional PVT models of reservoir fluids in multicomponent, multiphase hydrocarbon fields. These algorithms are specifically designed to operate under conditions of limited laboratory PVT data availability. Their implementation can significantly enhance the accuracy of reservoir flow simulations for fields with complex fluid compositions. The proposed methodology complements functioning advanced PVT-model calibration workflows and offers a reliable approach for modeling gas-condensate and oil-gas-condensate fluids with acceptable precision. The effectiveness of the approach is demonstrated through its application to fluids from an active gas-condensate field in the Republic of Uzbekistan.

#### REFERENCES

- [1]. Aliyev Z., Marakov D. "Development of Natural Gas Fields: A Textbook for Universities" – Moscow: MAX Press, 2011. – 340 p.
- [2]. Pyatibratov P. "Hydrodynamic Modeling of Oil Field Development: A Textbook for Universities" – Moscow: Gubkin Russian State University of Oil and Gas, 2015. – 167 p.
- [3]. Brusilovsky A.I. "Phase Transformations during Oil and Gas Field Development" – Moscow: Graal, 2002. – 575 p.
- [4]. Whitson C. "Characterizing Hydrocarbon Plus Fractions" // SPE Journal. – 1983, August. – pp. 683–694.
- [5]. Pedersen K., Fredenslund A., Thomassen P. "Properties of Oils and Natural Gases" – Houston: Gulf Publishing Company, 1989. – 253 p.
- [6]. Guzhov N., Buzinova O. "Challenges in Modeling Initial Compositions and Thermodynamic State of Gas-Condensate Field Systems" // Vesti Gazovoy Nauki. – 2014, no. 4(20). – pp. 64–72.

#### AUTHOR'S BIOGRAPHY



**Evstafeev Evgeniy Aleksandrovich** - Independent PhD candidate (Doctor of Philosophy in technical sciences), lecturer, Department of oil, gas and gas-condensate field development, Tashkent Branch of Gubkin Russian State University of Oil and Gas (National Research University).

Direction of activity - hydrodynamic modeling of multicomponent hydrocarbon reservoir development processes aimed at maximizing the recovery of valuable hydrocarbon fractions, combined with the application of multicriteria analysis and statistical decision theory to select the optimal field development strategy.

Has more than 20 scientific publications in national and foreign scientific and technical journals and conferences.



**Akramov Bakhshillo Shafievich** - Candidate of technical sciences, professor, Department of oil, gas and gas-condensate field development, Tashkent Branch of Gubkin Russian State University of Oil and Gas (National Research University)

Direction of activity - development and production of oil and gas fields, employing various enhanced oil recovery techniques to improve efficiency in exploiting hard-to-recover reserves.

Has more than 300 scientific publications in national and foreign scientific and technical journals and conferences, 2 monographs, 12 textbooks.



**Shevtsov Vladimir Mikhailovich** - Doctor of Technical Sciences (DSc), professor, Art. scientific co-workers, leading scientist co-workers design and monitoring department development of hydrocarbon deposits, JSC "O'ZLITINEFTGAZ"

Direction of activity - issues of increasing the efficiency of oil and gas and gas condensate field development, including deep-lying gas deposits with abnormally high pressures, the use of modern technologies for increasing hydrocarbon recovery from oil and gas and gas condensate fields.

Has more than 120 scientific publications in national and foreign scientific and technical journals and conferences, 2 monographs.



**Turaev Ulugbek Daminovich** – Deputy director for production, Mubarek Oil and Gas Production Department.

Direction of activity - hydrocarbon production from fields managed by the Mubarek Oil and Gas Production Department, overseeing initiatives to enhance productivity and carry out maintenance of oil and gas wells, as well as conducting hydrodynamic and gas–condensate studies on those wells.

Has more than 7 scientific publications in national and foreign scientific and technical journals and conferences.